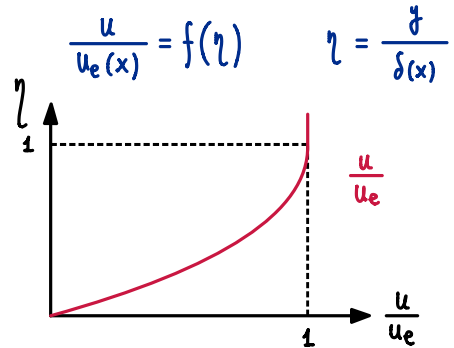


# Método de Pohlhausen

Si proponemos una cuártica para  $f(\eta)$ :

$$f(\eta) = C_0 + C_1\eta + C_2\eta^2 + C_3\eta^3 + C_4\eta^4$$

5 constantes  $\rightarrow$  5 condiciones: 
$$\begin{cases} \eta = 0 : f|_0 = 0 ; f''|_0 = -\Lambda \\ \eta = 1 : f|_1 = 1 ; f'|_1 = f''|_1 = 0 \end{cases}$$



POHLHAUSEN SEPARA EL EFECTO DE LA CURVATURA EN LA PARED ( $\Lambda$ ) DEL VALOR DE  $f$  EN  $\eta = 1$  :  $f = f_1 + \Lambda f_2$

Descomposición:

$$f_1 = \sum_{i=0}^4 C_{1i} \eta^i$$

$$f_1 = C_{10} + C_{11}\eta + C_{12}\eta^2 + C_{13}\eta^3 + C_{14}\eta^4$$

$$f_1' = C_{11} + 2C_{12}\eta + 3C_{13}\eta^2 + 4C_{14}\eta^3$$

$$f_1'' = 2C_{12} + 6C_{13}\eta + 12C_{14}\eta^2$$



$$\eta = 0 : f_1 = 0 ; f_1'' = 0$$

$$\eta = 1 : f_1 = 1 ; f_1' = 0 ; f_1'' = 0$$

$$\eta = 0 : \left\{ \begin{array}{l} C_{10} = 0 \\ C_{12} = 0 \end{array} \right\}$$

$$f_2 = \sum_{i=0}^4 C_{2i} \eta^i$$

$$f_2 = C_{20} + C_{21}\eta + C_{22}\eta^2 + C_{23}\eta^3 + C_{24}\eta^4$$

$$f_2' = C_{21} + 2C_{22}\eta + 3C_{23}\eta^2 + 4C_{24}\eta^3$$

$$f_2'' = 2C_{22} + 6C_{23}\eta + 12C_{24}\eta^2$$



$$\eta = 0 : f_2 = 0 ; f_2'' = -1$$

$$\eta = 1 : f_2 = 0 ; f_2' = 0 ; f_2'' = 0$$

$$\eta = 0 : \left\{ \begin{array}{l} C_{20} = 0 \\ C_{22} = -\frac{1}{2} \end{array} \right\}$$

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$$f_1 = 2\eta - 2\eta^3 + \eta^4$$

$$f_2 = \frac{1}{6}\eta(1-\eta)^3$$

Zona externa de la capa límite :

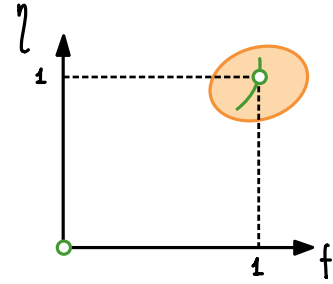
$$1 - \eta = \epsilon \quad (\epsilon \ll 1)$$

$$f_1 = 2\eta - 2\eta^3 + \eta^4 = 2(1-\epsilon) - 2(1-\epsilon)^3 + (1-\epsilon)^4 = 2 - 2\epsilon -$$

$$- 2(1 - 3\epsilon + 3\epsilon^2 - \epsilon^3) + (1 - 2\epsilon + \epsilon^2) = 2 - 2\epsilon - 2 + 6\epsilon - 6\epsilon^2 +$$

$$+ 2\epsilon^3 + 1 - 4\epsilon + 6\epsilon^2 - 4\epsilon^3 + \epsilon^4 = 1 - 2\epsilon^3 + \epsilon^4 \longrightarrow f_1 \approx 1 + O(\epsilon^3)$$

$$f_2 = \frac{1}{6}\eta(1-\eta)^3 = \frac{1}{6}(1-\epsilon)[1-(1-\epsilon)]^3 = \frac{1}{6}(1-\epsilon)\epsilon^3 = \frac{1}{6}\epsilon^3 - \frac{1}{6}\epsilon^4 \longrightarrow f_2 \approx \frac{\epsilon^3}{6} + O(\epsilon^4)$$



$$\frac{f_2}{f_1} \approx \frac{\epsilon^2}{6} \ll 1$$

EL EFECTO INTRODUCIDO POR LA CURVATURA NO AFECTA CASI EN ESTA ZONA

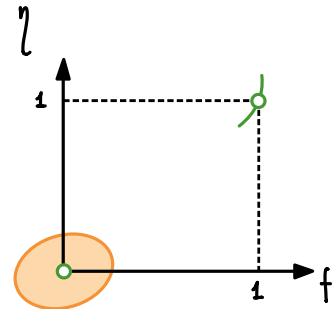
EN POHLHAUSEN LA REGIÓN EXTERIOR DE LA CAPA LÍMITE ES POCO SENSIBLE AL GRADIENTE DE PRESIONES, LO QUE CONLLEVARÁ CIERTO ERROR EN LOS RESULTADOS.

Cerca de la pared :

$$\eta = \epsilon \quad (\epsilon \ll 1)$$

$$f_1 = 2\eta - 2\eta^3 + \eta^4 = 2\epsilon - 2\epsilon^3 + \epsilon^4 \longrightarrow f_1 \approx 2\epsilon + O(\epsilon^3)$$

$$f_2 = \frac{1}{6}\eta(1-\eta)^3 = \frac{1}{6}(1 - 3\epsilon + 3\epsilon^2 - \epsilon^3) = \frac{\epsilon}{6} - \frac{\epsilon^2}{2} + \frac{\epsilon^3}{2} - \frac{\epsilon^4}{6} \longrightarrow f_2 \approx \frac{\epsilon}{6} + O(\epsilon^2)$$



$$\frac{f_2}{f_1} \approx \frac{1}{12}$$

Cerca de la pared, para que el efecto de  $\Lambda$  sea apreciable, debe ser  $\Lambda \sim O(10)$  : VARIACIONES IMPORTANTES CON RESPECTO A  $\Lambda = 0$  (Blasius).

Variaciones de orden unidad tendrían poca influencia cerca de la pared.

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$$= \eta \Big|_0^1 - \frac{2 + \frac{\Lambda}{6}}{2} \eta^2 \Big|_0^1 + \frac{\Lambda}{6} \eta^3 \Big|_0^1 + \frac{2 - \frac{\Lambda}{2}}{4} \eta^4 \Big|_0^1 - \frac{1 - \frac{\Lambda}{6}}{5} \eta^5 \Big|_0^1 = 1 - 1 - \frac{\Lambda}{12} + \frac{\Lambda}{6} + \frac{1}{2} -$$

$$- \frac{\Lambda}{8} - \frac{1}{5} + \frac{\Lambda}{30} = \frac{3}{10} - \frac{\Lambda}{120} \rightarrow \frac{\delta_1}{\delta} = \frac{1}{10} \left( 3 - \frac{\Lambda}{12} \right)$$

Espesor de cantidad de movimiento :

$$\delta_2 = \delta \int_0^1 f(1-f) d\eta \rightarrow \frac{\delta_2}{\delta} = \underbrace{\int_0^1 f d\eta}_I - \underbrace{\int_0^1 f^2 d\eta}_J$$

Resolvemos I :

$$I = \int_0^1 f d\eta = \int_0^1 d\eta - \int_0^1 (1-f) d\eta = 1 - \frac{1}{10} \left( 3 - \frac{\Lambda}{12} \right) \rightarrow I = \frac{1}{10} \left( 7 + \frac{\Lambda}{12} \right)$$

Resolvemos J :

$$J = \int_0^1 f^2 d\eta = \int_0^1 (f_1 + \Lambda f_2)^2 d\eta = \int_0^1 (f_1^2 + 2\Lambda f_1 f_2 + \Lambda^2 f_2^2) d\eta = \underbrace{\int_0^1 f_1^2 d\eta}_{J_1} + 2\Lambda \underbrace{\int_0^1 f_1 f_2 d\eta}_{J_2} + \Lambda^2 \underbrace{\int_0^1 f_2^2 d\eta}_{J_3}$$

$$J_1 = \int_0^1 f_1^2 d\eta = \int_0^1 (2\eta - 2\eta^3 + \eta^4)^2 d\eta = \int_0^1 (4\eta^2 - 4\eta^4 + 2\eta^5 - 4\eta^4 + 4\eta^6 - 2\eta^7 + 2\eta^5 - 2\eta^7 + \eta^8) d\eta = \frac{4}{3} - \frac{4}{5} + \frac{1}{3} - \frac{4}{5} + \frac{4}{7} - \frac{1}{4} + \frac{1}{3} - \frac{1}{4} + \frac{1}{9} = \frac{367}{630} \rightarrow J_1 = \frac{367}{630}$$

$$J_2 = 2\Lambda \int_0^1 f_1 f_2 d\eta = 2\Lambda \int_0^1 (2\eta - 2\eta^3 + \eta^4) \frac{1}{6} \eta (1-\eta)^3 d\eta \xrightarrow{\text{CASIO}} J_2 = \frac{71}{7560} \Lambda$$

$$J_3 = \Lambda^2 \int_0^1 f_2^2 d\eta = \Lambda^2 \int_0^1 \frac{1}{36} \eta^2 (1-\eta)^6 d\eta = \xrightarrow{\text{CASIO}} J_3 = \frac{1}{9072} \Lambda^2$$

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$$\rightarrow \frac{\delta_2}{\delta} = \frac{63}{63} - \frac{1}{5} - \frac{\Lambda}{5 \cdot 12} - \left( \frac{\Lambda}{12} \right)$$

Factor de forma:

$$H_{12} = \frac{\delta_1}{\delta_2} = \frac{\frac{\delta_1}{\delta}}{\frac{\delta_2}{\delta}} = \frac{\frac{1}{10} \left( 3 - \frac{\Lambda}{12} \right)}{\frac{1}{63} \left[ \frac{37}{5} - \frac{4}{5} \frac{\Lambda}{12} - \left( \frac{\Lambda}{12} \right)^2 \right]} \rightarrow H_{12} = \frac{63}{10} \frac{3 - \frac{\Lambda}{12}}{\frac{37}{5} - \frac{4}{5} \frac{\Lambda}{12} - \left( \frac{\Lambda}{12} \right)^2}$$

Coefficiente de fricción:

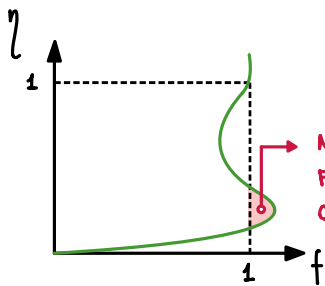
$$\frac{C_f}{2} = \frac{\nu}{u_e \delta} \left. \frac{df}{d\eta} \right|_{\eta=0} = \frac{\nu}{u_e \delta} \frac{d}{d\eta} \left[ 2\eta - 2\eta^3 + \eta^4 + \Lambda \frac{1}{6} \eta (1-\eta)^3 \right]_{\eta=0} = \frac{\nu}{u_e \delta} \left[ 2 - 6\eta + \right.$$

$$\left. + 4\eta^3 - \frac{\Lambda}{2} \eta (1-\eta)^2 + \frac{\Lambda}{6} (1-\eta)^3 \right]_{\eta=0} = \frac{\nu}{u_e \delta} \left( 2 + \frac{\Lambda}{6} \right) \rightarrow \frac{C_f}{2} = \frac{2\nu}{u_e \delta} \left( 1 + \frac{\Lambda}{12} \right)$$

Si  $\Lambda = -12$ :  $C_f = 0$  (SEPARACIÓN EN POHLHAUSEN)  $\rightarrow \Lambda \geq -12$  CONDICIÓN NECESARIA 

Pohlhausen no sirve si  $\Lambda < -12$  porque implicaría curvatura negativa de la pared  $\rightarrow$  flujo reverso

Para  $\Lambda > 12 \exists \eta^*/f(\eta^*) > 1$ :



$$\rightarrow \Lambda \leq 12 \rightarrow -12 \leq \Lambda \leq 12 \rightarrow -1 \leq \frac{\Lambda}{12} \leq 1$$

Hay otro parámetro interesante:

$$\lambda = \frac{\delta_2^2}{\nu} \frac{du_e}{dx}$$

$$-0'1567 \leq \lambda \leq 0'0948$$

$$\lambda = \left( \frac{\delta_2}{\delta} \right)^2 \frac{du_e}{dx} \frac{\delta^2}{\nu} = \frac{\Lambda}{3969} \left[ \frac{37}{5} - \frac{4}{5} \frac{\Lambda}{12} - \left( \frac{\Lambda}{12} \right)^2 \right]^2 \rightarrow \lambda = \frac{\Lambda}{3969} \left[ \frac{37}{5} - \frac{4}{5} \frac{\Lambda}{12} - \left( \frac{\Lambda}{12} \right)^2 \right]^2$$

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y entonces:



Ecuación de Karman:

$$\frac{d\delta_2}{dx} + \underbrace{(2 + H_{12}) \frac{1}{u_e} \frac{du_e}{dx}}_0 \delta_2 = \frac{C_f}{2} \rightarrow \frac{37}{315} \frac{d\delta}{dx} = \frac{2\sqrt{}}{u_e \delta} \rightarrow \int_0^\delta \tilde{\delta} d\tilde{\delta} = \int_0^x \left[ \frac{630}{37} \frac{\sqrt{}}{u_e} \right] dx \xrightarrow{\delta(0)=0}$$

$$\rightarrow \frac{\delta^2}{2} = \frac{630}{37} \frac{\sqrt{}}{u_e} x \rightarrow \boxed{\frac{\delta}{x} = 6 \sqrt{\frac{35}{37}} Re_x^{-1/2}}$$

Con  $\frac{\delta}{x}$  podemos obtener  $\frac{\delta_1}{x}$ ,  $\frac{\delta_2}{x}$  y  $\frac{C_f}{2}$ :

$$\frac{\delta_1}{x} = \frac{3}{10} \frac{\delta}{x}$$

$$\boxed{\frac{\delta_1}{x} = \frac{9}{5} \sqrt{\frac{35}{37}} Re_x^{-1/2} \approx 1.751 Re_x^{-1/2}}$$

En la solución exacta de Blasius era  $1.721 Re_x^{-1/2} \rightarrow 1.7\%$  de error

$$\frac{\delta_2}{x} = \frac{37}{315} \frac{\delta}{x}$$

$$\boxed{\frac{\delta_2}{x} = \frac{74}{105} \sqrt{\frac{35}{37}} Re_x^{-1/2} \approx 0.685 Re_x^{-1/2}}$$

En la solución exacta de Blasius era  $0.664 Re_x^{-1/2} \rightarrow 3.2\%$  de error

Karman

$$\frac{C_f}{2} = \frac{d\delta_2}{dx} = \frac{d}{dx} \left( \frac{74}{105} \sqrt{\frac{35}{37}} \sqrt{\frac{\sqrt{x}}{u_e}} \right) = \frac{74}{105} \sqrt{\frac{35}{37}} \sqrt{\frac{\sqrt{}}{u_e}} \frac{1}{2\sqrt{x}}$$

$$\boxed{\frac{C_f}{2} = \frac{74}{105} \sqrt{\frac{35}{37}} Re_x^{-1/2} \approx 0.685 Re_x^{-1/2}}$$

Blasius:  $0.664 Re_x^{-1/2}$  (3.2% error)

A la vista de los errores, Pohlhausen es una buena aproximación de la solución de Blasius.

### VALIDACIÓN CON FALKNER - SKAN

Por último, vamos a ver cómo de bueno es este método para capa límite con gradiente de presiones.

Ecuación de Karman:

$$\frac{d\delta_2}{dx} + (2 + H_{12}) \frac{1}{u_e} \frac{du_e}{dx} \delta_2 = \frac{C_f}{2} \xrightarrow{\cdot \frac{u_e \delta_2}{\sqrt{}}} \frac{u_e \delta_2}{\sqrt{}} \frac{d\delta_2}{dx} + (2 + H_{12}) \lambda = \frac{C_f}{2} \frac{u_e}{\sqrt{}} \delta_2 \xrightarrow{\downarrow}$$

$$\rightarrow \frac{u_e}{\sqrt{}} \frac{d\left(\frac{\delta_2^2}{2}\right)}{dx} + (2 + H_{12}) \lambda = \frac{\delta_2}{\delta} \cdot 2 \left(1 + \frac{\Lambda}{12}\right) \xrightarrow{\frac{\delta_2^2}{\sqrt{}} = \frac{\lambda}{du_e/dx}} u_e \frac{d}{dx} \left( \frac{\lambda}{du_e/dx} \right) = 2 \left[ T(\lambda) - (2 + H_{12}) \lambda \right]$$

$T(\lambda)$   $F(\lambda)$

Por tanto:

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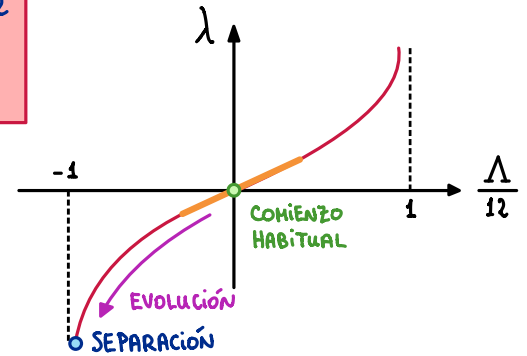
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Dado que  $\frac{\lambda}{\Lambda} = \frac{\delta}{\delta_2} \rightarrow$

$$\lambda = \frac{\Lambda}{63^2} \left[ \frac{37}{5} - \frac{4}{5} \frac{\Lambda}{12} - \left( \frac{\Lambda}{12} \right)^2 \right]^2$$

Si tenemos una aceleración/deceleración moderada ( $\Lambda \sim 1$ ), la

relación entre  $\lambda$  y  $\Lambda$  se hace lineal:  $\lambda \approx \left( \frac{37}{315} \right)^2 \Lambda$



Al igual que analizamos la separación, también analizamos la presencia de un punto de remanso ( $u_e = 0$ ).

Si  $u_e = 0$  no podemos arrancar la solución, y para solucionarlo recurrimos a la solución de Falkner - Skan:

$$u_e = Ax^m \quad (m > 0) \rightarrow \frac{du_e}{dx} = mA x^{m-1} \rightarrow \frac{1}{du_e/dx} = \frac{1}{m} \frac{x^{1-m}}{A}$$

$$Ax^m \frac{d}{dx} \left( \frac{\lambda}{mA} x^{1-m} \right) = F(\lambda)$$

$$x^m \frac{d}{dx} (\lambda x^{1-m}) = m F(\lambda)$$

$$x^m \frac{d\lambda}{dx} x^{1-m} + x^m \lambda (1-m) x^{-m} = m F(\lambda)$$

$$x \frac{d\lambda}{dx} + \lambda (1-m) = m F(\lambda)$$

LA EVOLUCIÓN DE  $\lambda$  SIGUE ESTA ECUACIÓN DIFERENCIAL

**NOTA**

$$\lambda = \frac{\delta_2^2}{\delta_2} \frac{du_e}{dx}$$

Falkner - Skan:  $\begin{cases} \frac{\delta_2}{x} = cte(m) \cdot Re_x^{-1/2} \\ u_e = Ax^m; \frac{du_e}{dx} = \frac{m u_e}{x} \end{cases}$

$$\lambda = \frac{cte(m) x^2}{\sqrt{Re_x}} \frac{du_e}{dx} = cte(m) \frac{x^2}{\sqrt{\frac{u_e x}{\nu}}} \frac{m u_e}{x} = m cte(m) \rightarrow \lambda = cte(m)$$

POHLHAUSEN ES CONSISTENTE CON FALKNER - SKAN

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$x = x_0 : \lambda = \lambda_0$  ¡OJO! ESTAR CERCA DEL PR ( $u_e = 0$ ) NO ES LO MISMO

¡OJO! ESTAR CERCA DEL PR ( $u_e = 0$ ) NO ES LO MISMO

$$\frac{\Lambda}{12} = -1$$

En cuanto a la separación :  $\lambda_{s-p} = -0'1567$  (Pohlhausen) ;  $\lambda_{s-fs} = -0'067$  (Falkner - Skan)

EL ERROR ES MUY GRANDE EN LA ZONA DE SEPARACIÓN PORQUE EL MÉTODO DE POHLHAUSEN ES POCO SENSIBLE AL GRADIENTE DE PRESIONES DEL FLUJO EXTERIOR (DEMASIADO OPTIMISTA)

Tabla resumen de resultados :

$\frac{\Lambda}{12}$	$\lambda_p$	$\lambda_{fs}$	$T(\lambda)$	$H_{12}(\lambda)$	$F(\lambda)$
-1	-0'1567	-0'067	0	3'5	1'72
0	0	0	0'2349	2'55	0'47
1	0'0948	<del>0</del>	0'3556	2'25	-0'0948

SEPARACIÓN POHLHAUSEN

BLASIUS

MÁXIMA ACELERACIÓN COMPATIBLE CON QUE NO HAYA SOBREVELOCIDADES DENTRO DE LA CAPA LÍMITE.

NO CAMBIA DEMASIADO, ESPECIALMENTE EN LA ZONA DE ACELERACIÓN ( $\frac{dU_e}{dx} > 0$ , es decir,  $\lambda > 0$ ).

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